

1 Replicate Error

Replicates: $\{x_1, x_2, \dots, x_n\}$

$$s^2 = \frac{1}{n-1} \sum_{i=1}^n (x_i - \bar{x})^2$$

$$e_{s,rep} = \frac{s}{\sqrt{n}}$$

$$\alpha \equiv (1 - \mathbb{P}) \quad \mathbb{P} \in [0, 1]$$

$$\nu = n - 1$$

$$t_{\alpha,\nu} = |\text{T.INV.}2\text{T}(\alpha, \nu)|$$

$$\text{CI}(\mathbb{P}) = \bar{x} \pm t_{\alpha,\nu} e_{s,rep}$$

2 Process Control

$$K_p = \frac{\Delta y^\ominus}{\Delta u^\ominus}$$

$$\tau \equiv \{t|y(t) = y_0 + 0.632\Delta y^\ominus\}$$

$$\tau_p \equiv \tau - t_{\text{response}}$$

$$\theta_p \equiv t_{\text{step}} - t_{\text{response}}$$

$$\text{PB} \equiv \frac{100}{K_c}$$

3 Mass Transport

$$\dot{V} = A_\sigma \langle \vec{v} \rangle \quad \dot{V} = \frac{\dot{m}}{\rho}$$

$$\rho_1 A_{\sigma 1} \langle \vec{v}_1 \rangle = \rho_2 A_{\sigma 2} \langle \vec{v}_2 \rangle$$

$$\langle \vec{v}_z \rangle = \sqrt{2gz} \quad \vec{v}_t = 2\pi R f$$

$$\frac{\Delta P}{\rho} + \frac{\Delta(\vec{v}^2)}{2\alpha} + g\Delta z + \sum \hat{F} = \frac{\dot{W}_{s,by}}{\dot{m}} \quad \alpha \approx 1, \text{ turbulent} \\ \alpha = 0.5, \text{ laminar}$$

$$\sum \hat{F} = \sum_i 4f_i \frac{\ell_i}{\varnothing_i} \left(\frac{\langle \vec{v} \rangle_i^2}{2} \right) + \sum_j K_{f,j} \left(\frac{\langle \vec{v} \rangle_j^2}{2} \right)$$

$$z_1 g + \frac{\vec{v}_1^2}{2} + \frac{P_1}{\rho} = z_2 g + \frac{\vec{v}_2^2}{2} + \frac{P_2}{\rho}$$

$$\eta_{\text{pump}} = \frac{\dot{W}_s}{\dot{W}_{\text{pump}}} \quad -\dot{W}_s = \dot{H}g \quad P_{\text{brake}} = \frac{-\dot{W}_s}{\eta} \dot{m}$$

$$\tilde{H} = \frac{P}{\gamma} \quad \gamma \equiv \rho g$$

$$\Delta P_{\text{pipe}} = 4f\rho \frac{\ell}{\varnothing} \frac{\vec{v}^2}{2} \quad \Delta P_{\text{pipe,lam}} = \frac{32\mu \vec{v} \ell}{\varnothing^2}$$

$$\hat{F}_{\text{pipe}} = \frac{\Delta P_{\text{pipe}}}{\rho} = 4f \frac{\ell}{\varnothing} \frac{\langle \vec{v} \rangle^2}{2} \quad \hat{F}_{\text{fitting}} = K_f \frac{\langle \vec{v} \rangle^2}{2}$$

$$\text{Re} = \frac{\langle \vec{v} \rangle \rho \varnothing}{\mu} \quad \text{Laminar: } f = 16/\text{Re}$$

$$K_{\text{expansion}} = \left(1 - \frac{A_{\sigma 1}}{A_{\sigma 2}} \right)^2 \quad \hat{F}_{\text{expansion}} = K_{\text{expansion}} \frac{\langle \vec{v}_1 \rangle^2}{2\alpha}$$

$$K_{\text{contraction}} = 0.55 \left(1 - \frac{A_{\sigma 2}}{A_{\sigma 1}} \right) \quad \hat{F}_{\text{contraction}} = K_{\text{contraction}} \frac{\langle \vec{v}_2 \rangle^2}{2\alpha}$$

$$\text{NPSH}_A = \frac{P - p^*}{\rho g} + z - \tilde{H}_v - \frac{\sum \hat{F}}{g} \quad \tilde{H}_v = \frac{\vec{v}^2}{2g}$$

$$\frac{\dot{V}_1}{\dot{V}_2} = \frac{\dot{N}_{r,1}}{\dot{N}_{r,2}} \quad \frac{\tilde{H}_1}{\tilde{H}_2} = \frac{\dot{V}_1^2}{\dot{V}_2^2} = \frac{\dot{N}_{r,1}^2}{\dot{N}_{r,2}^2} \quad \frac{\dot{W}_1}{\dot{W}_2} = \frac{\tilde{H}_1 \dot{V}_1}{\tilde{H}_2 \dot{V}_2} = \frac{\dot{N}_{r,1}^3}{\dot{N}_{r,2}^3}$$

$$\text{Gas: } p_1^2 - p_2^2 = \frac{4f\ell\Phi_G^2 RT}{\varnothing \dot{m}}$$

4 2² Factorial Design

$$E_i = \bar{y}_{i+} - \bar{y}_{i-} = \frac{C_i}{2^{(N_L-1)n}} = \frac{C_i}{2n} \quad E_{ij} = \frac{C_{AB}}{2^{(N_L-1)n}} = \frac{C_{AB}}{2n}$$

$$C_A = a+ab-b-(1) \quad C_B = b+ab-a-(1) \quad C_{AB} = ab+(1)-a-b$$

$$\text{SS}_i = \frac{C_i^2}{2^{(N_L)n}} = \frac{C_i^2}{4n}$$

$$\text{SST} = \sum_{i=1}^{N_L} \sum_{j=1}^{N_L} \sum_{k=1}^n (y_{ijk})^2 - \frac{(\sum y_{ijk})^2}{4n}$$

$$\text{SSE} = \text{SST} - \sum \text{SS}_i$$

$$\nu_i = N_{L,i} - 1 \quad \nu_{\text{SSE}} = 4(n-1) \quad \nu_{\text{SST}} = 4n - 1$$

$$\text{MS}_i = \frac{\text{SS}_i}{\nu_i} \quad \text{MSE} = \frac{\text{SSE}}{\nu_{\text{SSE}}} \quad F_{0,i} = \frac{\text{MS}_i}{\text{MSE}}$$

$$\alpha = 1 - \frac{\% \text{CI}}{100} \quad F_{c,i} = \text{FINV}(\alpha, \nu_i, \nu_{\text{SSE}}) \quad p = \text{FDIST}(F_{0,i}, \nu_i, \nu_{\text{SSE}})$$

$$\hat{y} = \hat{\beta}_0 + \hat{\beta}_1 x_1 + \hat{\beta}_2 x_2 + \hat{\beta}_{12} x_1 x_2 + \varepsilon$$

$$\hat{\beta}_0 = \frac{\sum y_{ijk}}{n} \quad \hat{\beta}_1, \hat{\beta}_2, \hat{\beta}_{12} = \frac{E_i}{|x_1 - x_2|}$$

$$e_i = y_i - \hat{y}_i \quad e_{s,\beta} = \sqrt{\frac{\text{MSE}}{2^{N_L} n}} \quad t_i = \frac{\hat{\beta}_i}{e_{s,\beta}}$$

5 Statistical Process Control

$$\bar{R} = \frac{\sum_i^n R_i}{n}$$

$$\text{UCL}_R = D_4 \bar{R} = \bar{R} + \frac{3d_3 \bar{R}}{d_2}$$

$$\text{LCL}_R = D_3 \bar{R} = \bar{R} - \frac{3d_3 \bar{R}}{d_2}$$

$$D_4 \equiv 1 + \frac{3d_3}{d_2} \quad D_3 \equiv 1 - \frac{3d_3}{d_2} \quad d_2 = \frac{\bar{R}}{\sigma_x} \quad d_3 = \frac{\sigma_R}{\sigma_x}$$

$$\bar{\bar{x}} = \frac{\sum_i^n \bar{x}_i}{n}$$

$$\text{UCL}_{\bar{x}} = \bar{\bar{x}} + \frac{3\sigma}{\sqrt{n}}$$

$$\text{LCL}_{\bar{x}} = \bar{\bar{x}} - \frac{3\sigma}{\sqrt{n}}$$

$$\text{Unknown } \sigma : \hat{\sigma} = \frac{\bar{R}}{d_2} \quad A_2 \equiv \frac{3}{d_2 \sqrt{n}}$$

$$\text{UCL}_{\bar{x}} = \bar{\bar{x}} + \frac{3}{d_2 \sqrt{n}} \bar{R} = \bar{\bar{x}} + A_2 \bar{R}$$

$$\text{LCL}_{\bar{x}} = \bar{\bar{x}} - \frac{3}{d_2 \sqrt{n}} \bar{R} = \bar{\bar{x}} - A_2 \bar{R}$$

$$\text{Cp} \equiv \frac{\text{USL} - \text{LSL}}{6\sigma}$$

References

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